

# Low Distortion Rail-to-Rail Amplifiers Drive ADCs and Cables

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## Introduction

Operating from supplies as low as 2.5V, the 325MHz LT1806 and the 180MHz LT1809 rail-to-rail amplifiers provide the distortion and noise performance required by low voltage signal conditioning and data acquisition systems. Rail-to-rail inputs and outputs allow the entire supply range to be used, and the high output current capability, 60mA typical on a 3V supply, is ideal for cable-driver applications. The LT1806 is optimized for noise and DC performance, featuring a low voltage noise of 3.5nV/√Hz and a maximum offset voltage of 550μV. The LT1809 is optimized for slew rate and distortion, featuring a slew rate of 350V/μs and low harmonic distortion

tion -90dBc at  $f_c = 5\text{MHz}$  ( $V_S = 5\text{V}$ ,  $V_O = 2V_{P-P}$ ). Both parts are fully specified for 3V, 5V and ±5V operation and are available in 8-lead SO and 6-lead SOT-23 packages. A shutdown function is included that disables the amplifier and reduces the supply current to less than 1mA.

## Performance

Table 1 summarizes the performance of the LT1806 and LT1809. Note that input offset voltage is specified at both the positive and negative supply rails, in contrast to most competitive parts, which are only specified at mid-supply.

Table 1. LT1806/LT1809 key performance specifications

Parameter	LT1806	LT1809
Gain-Bandwidth Product	325MHz	180MHz
Slew Rate	140V/μs	350V/μs
Input Voltage Noise	3.5nV/√Hz	16nV/√Hz
Harmonic Distortion, $R_L = 1k$ $f_c = 5\text{MHz}$ , $V_S = 5\text{V}$ , $A_V = 1$ , $V_O = 2V_{P-P}$	-80dBc	-90dBc
Settling Time 0.01% $V_{STEP} = 2\text{V}$ , $V_S = 5\text{V}$ , $A_V = 1$	60ns	40ns
Operating Supply Range	2.5V to 12V	2.5V to 12V
Output Swing High $I_L = 5\text{mA}$ $I_L = 25\text{mA}$	$V_S - 0.18\text{V Max}$ $V_S - 0.7\text{V Max}$	$V_S - 0.16\text{V Max}$ $V_S - 0.5\text{V Max}$
Output Swing Low $I_L = 5\text{mA}$ $I_L = 25\text{mA}$	0.13V Max 0.4V Max	0.08V Max 0.3V Max
Short Circuit Current, $V_S = 3\text{V}$	±30mA Min	±40mA Min
Input Offset Voltage $V_{CM} = V^+$ , $V^-$	0.55mV Max	2.5mV Max
Input Bias Current	13μA Max	28μA Max
CMRR $V_S = 5\text{V}$ , $V_{CM} = V^+$ to $V^-$	80dB Min	69dB Min
PSRR $V_S = 2.5\text{V to } 10\text{V}$ , $V_{CM} = 0\text{V}$	91dB Min	73dB Min
Supply Current, $V_S = 5\text{V}$	13mA Max	17mA Max
Supply Current, $V_S = 5\text{V Shutdown}$	0.9mA Max	0.8mA Max

The distortion vs frequency for the two parts is shown in Figures 1–4. The harmonic distortion was measured with two loads: 100Ω, which is representative of a cable-driving application, and 1kΩ, which is typical of signal-conditioning applications. Both devices are quite good but the LT1809 provides the ultimate in distortion performance.

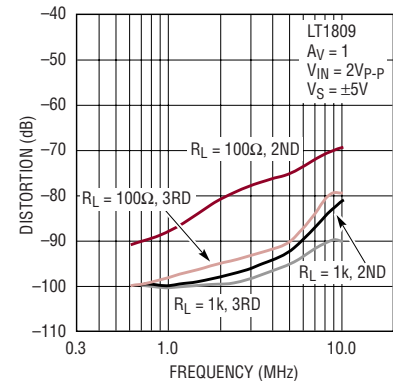


Figure 1. LT1809 distortion vs frequency

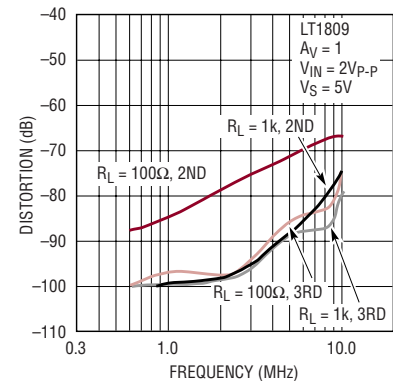
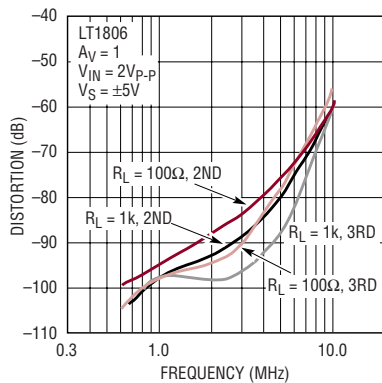


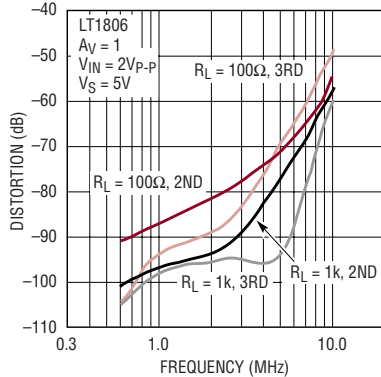
Figure 2. LT1809 distortion vs frequency

## Single 3V Supply, 4MHz, 4th Order Butterworth Filter

A low distortion, low voltage filter, suitable for antialiasing applications, is shown in Figure 5. The filter is a cascade of two inverting 2nd order sections, with values selected to give a Butterworth response. In this configuration, signal swing on the inputs of the op amps is small, resulting in



**Figure 3. LT1806 distortion vs frequency**

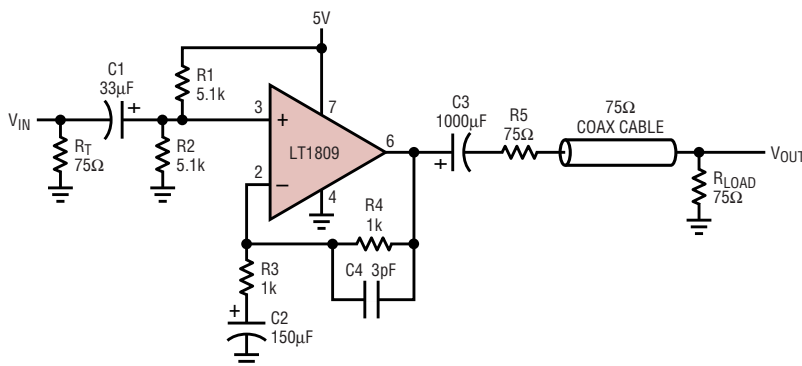


**Figure 4. LT1806 distortion vs frequency**

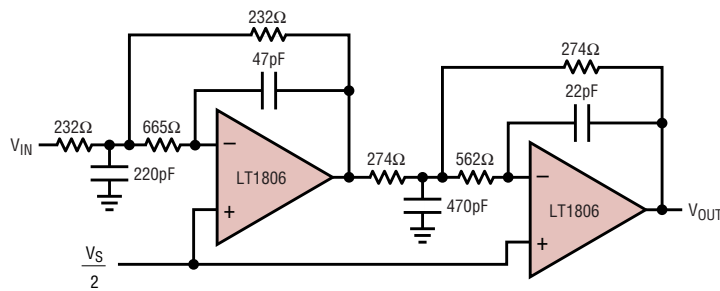
good distortion performance. Distortion was measured at  $-83\text{dBc}$  at  $1\text{MHz}$ ,  $V_O = 2.25V_{P-P}$ . The overall filter response (Figure 6) shows a stopband that has greater than  $95\text{dB}$  rejection of frequencies up to  $100\text{MHz}$ . Such stopband depth would be difficult to achieve with a dual op amp because of crosstalk and layout issues.

### Single 5V Supply Video-Cable Driver

The high output current capability of the LT1809 can be put to use in video-cable-driver applications. Figure 7



**Figure 7. Single-supply video line driver**

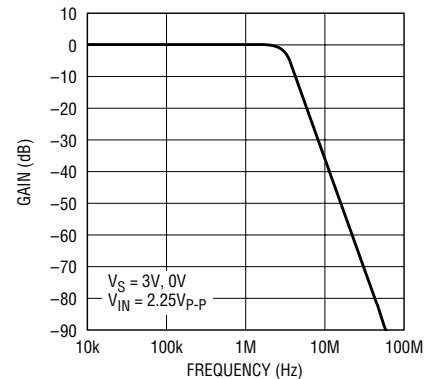


**Figure 5. Single 3V supply, 4MHz, 4th order Butterworth filter**

shows an AC-coupled video driver using a single 5V supply. The input signal is level shifted to half supply by coupling capacitor C1 and resistor divider R1/R2. An AC gain of two in the amplifier, set by resistors R3 and R4 and capacitor C2, compensates for the loss due to the output termination resistors R5 and  $R_{LOAD}$ , resulting in an overall gain of one. Figure 8 shows the frequency response of the driver. The  $-3\text{dB}$  bandwidth is about  $95\text{MHz}$  and peaking is less than  $1\text{dB}$ .

### Buffering Data Converters

Driving ADCs is a tricky business. Looking at the circuit of Figure 9, you would correctly surmise that the signal flows from left to right. Entering the noninverting input, this signal takes a gain of 2 in the LT1809. It passes through the  $6.8\text{MHz}$  lowpass filter formed by R3 and C1 and is applied to the LTC1420 ADC. With the  $10\text{Msps}$ , 12-bit LTC1420 set in a gain of 1 and its internal reference set at  $2.048\text{V}$ , the full-scale signal is about  $1V_{P-P}$ , input referred. Figure 10, a 4096 point FFT, shows results

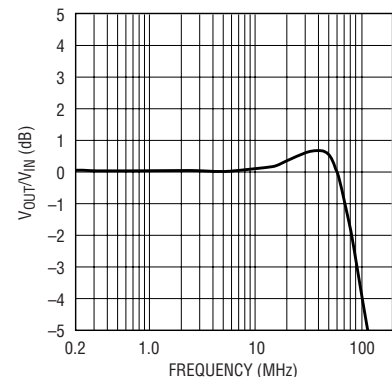


**Figure 6. Frequency response of Figure 5's filter**

achieved with a  $1.394\text{MHz}$  signal. The spurious free dynamic range is about  $90\text{dB}$ , with performance limited by the ADC's nonlinearities rather than by the LT1809. (Typical SFDR for the LTC1420 is  $83\text{dB}$ .)

However, there is also a signal, the ADC sampling glitch, that travels from right to left. It is caused by a small flying sample capacitor in the ADC front end, which introduces an AC short circuit at the ADC's input ten million times per second. This signal

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**Figure 8. Frequency response of Figure 7's circuit**

can cause grief to upstream circuitry unless means are taken to attenuate it. The LT1809 performs admirably in this task. Tracing the reverse signal path from the LTC1420, C1 serves as a storage capacitor and R3 limits the glitch current into the LT1809's output. The LT1809's collector output stage incorporates proprietary local feedback to reduce its output impedance (about  $20\Omega$  at 100MHz) and this helps attenuate the glitch as well. However, a remnant glitch persists and works its way through R2 and R1, being attenuated by a factor of 2 in the process, and arrives at the

LT1809 inverting input. For best performance, the amplitude of the glitch at this point should have been reduced to several millivolts. If it is larger than about 25mV, the rule-of-thumb for BJT differential pairs, the input stage will begin to be driven outside of its linear region and excess distortion will result. The excellent results of Figure 10 indicate that the circuit is not suffering from this effect.

## Conclusion

The LT1806 and LT1809 provide complementary solutions for high speed, low voltage signal conditioning. The LT1806, with its low voltage

noise of  $3.5\text{nV}/\sqrt{\text{Hz}}$  and a maximum offset voltage of  $550\mu\text{V}$ , is ideal for applications requiring low noise or DC precision, whereas the LT1809 provides the ultimate in distortion performance. The rail-to-rail inputs and outputs of the devices maximize dynamic range and can simplify designs by eliminating the need for a negative supply. This combination of features in a SOT-23 package makes the devices a top choice for handling the challenges of low voltage signal conditioning. 

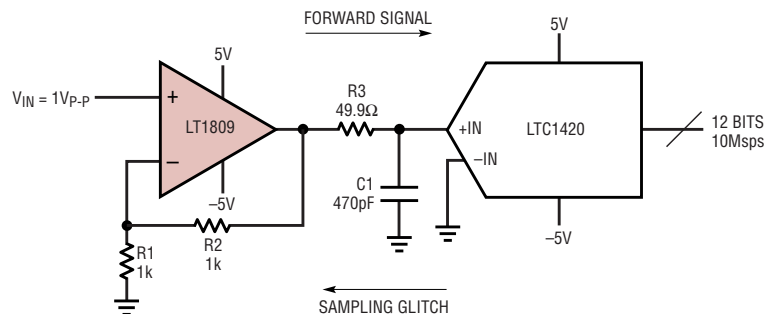


Figure 9. High speed ADC driver

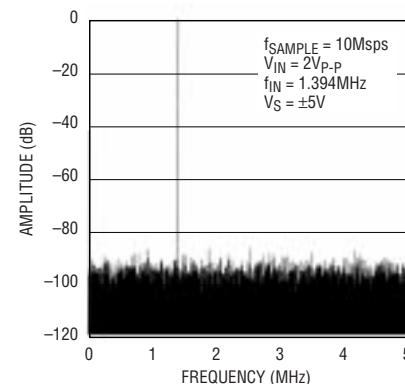


Figure 10. 4096 point FFT of the 12-bit ADC's output